

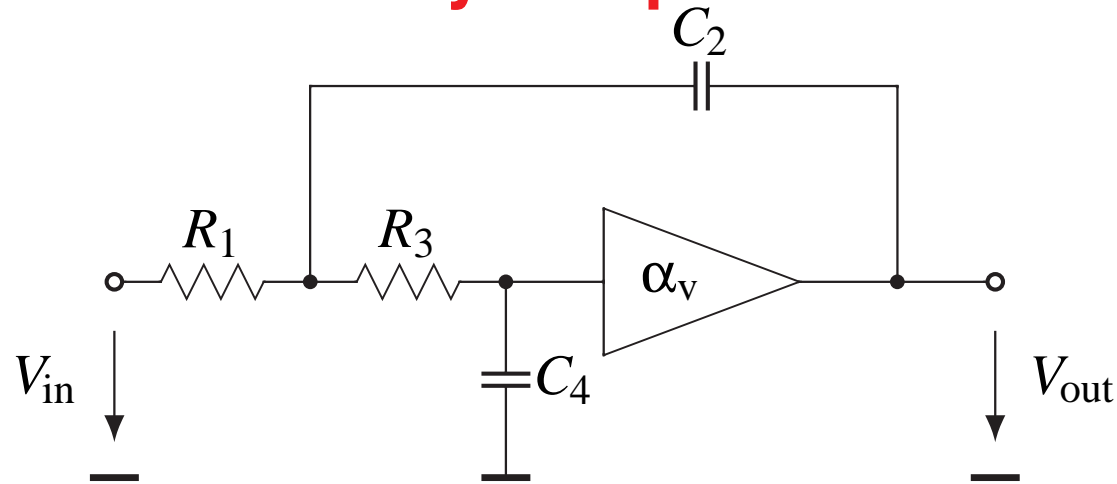
**MINIMUM-SENSITIVITY
SINGLE-AMPLIFIER BIQUADRATIC FILTERS**

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**GENERAL CASE: GAIN BELOW TWO.
UNITY-GAIN: SOME FILTERS NEED LOW COMPONENT SPREADS.**

ECCTD 1999, SEPTEMBER 2, STRESA, ITALY.

Sallen-Key Lowpass Filter

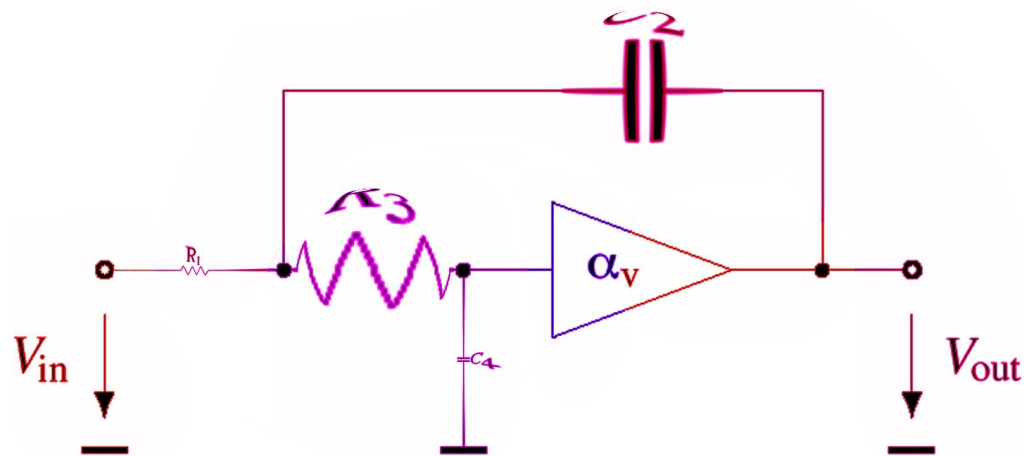
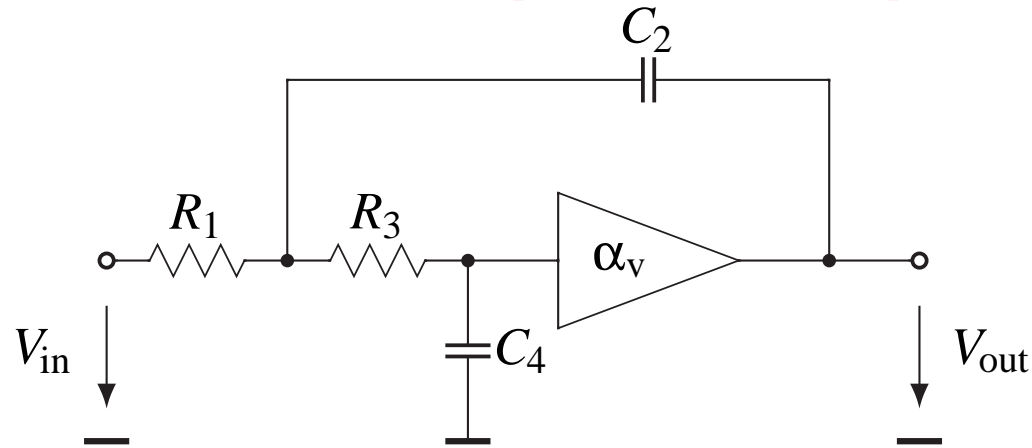


(with $R_1 = R/n$, $R_3 = R \cdot n$, $C_2 = C/m$ and $C_4 = C \cdot m$)

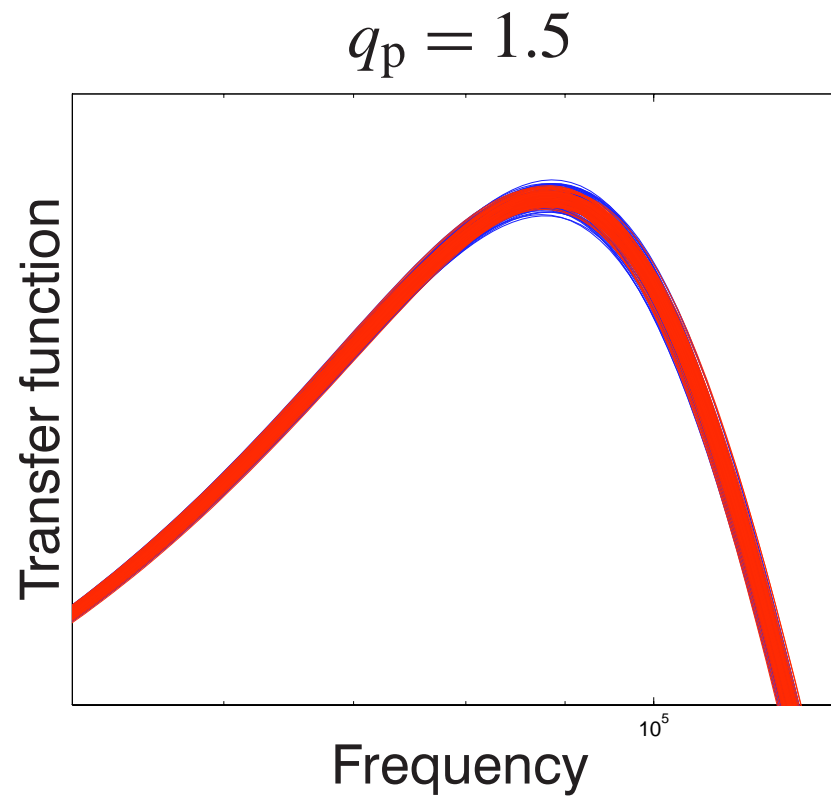
$$T(s) = \alpha_V \frac{\omega_p^2}{s^2 + \frac{\omega_p}{q_p} s + \omega_p^2}$$

$$\omega_p = \frac{1}{RC}, \quad \frac{1}{q_p} = mn + \frac{m}{n} + \frac{1 - \alpha_V}{mn}$$

General case: Impedance tapering



Unity-gain filter: Low component spreads

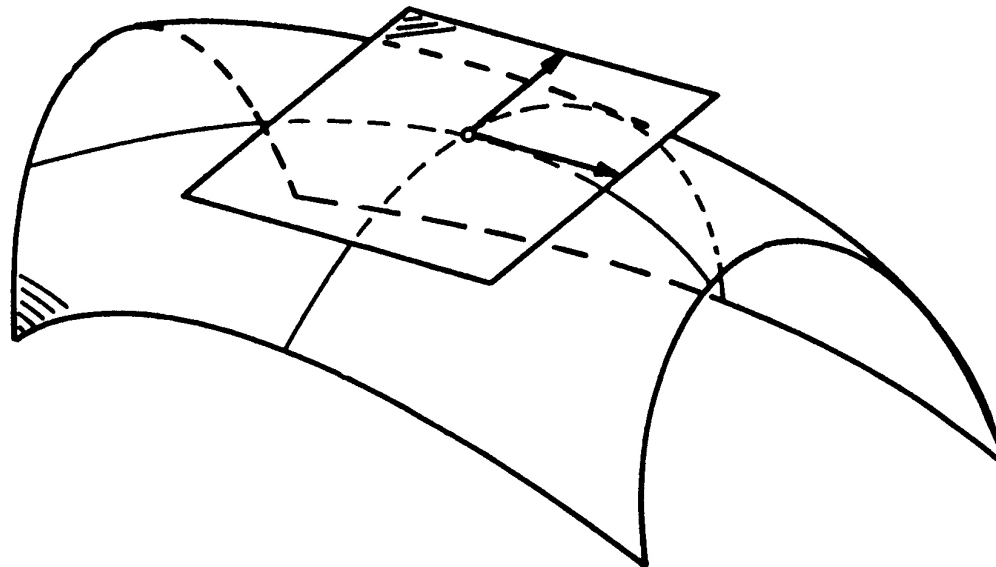


Very large and **very low** component spreads.

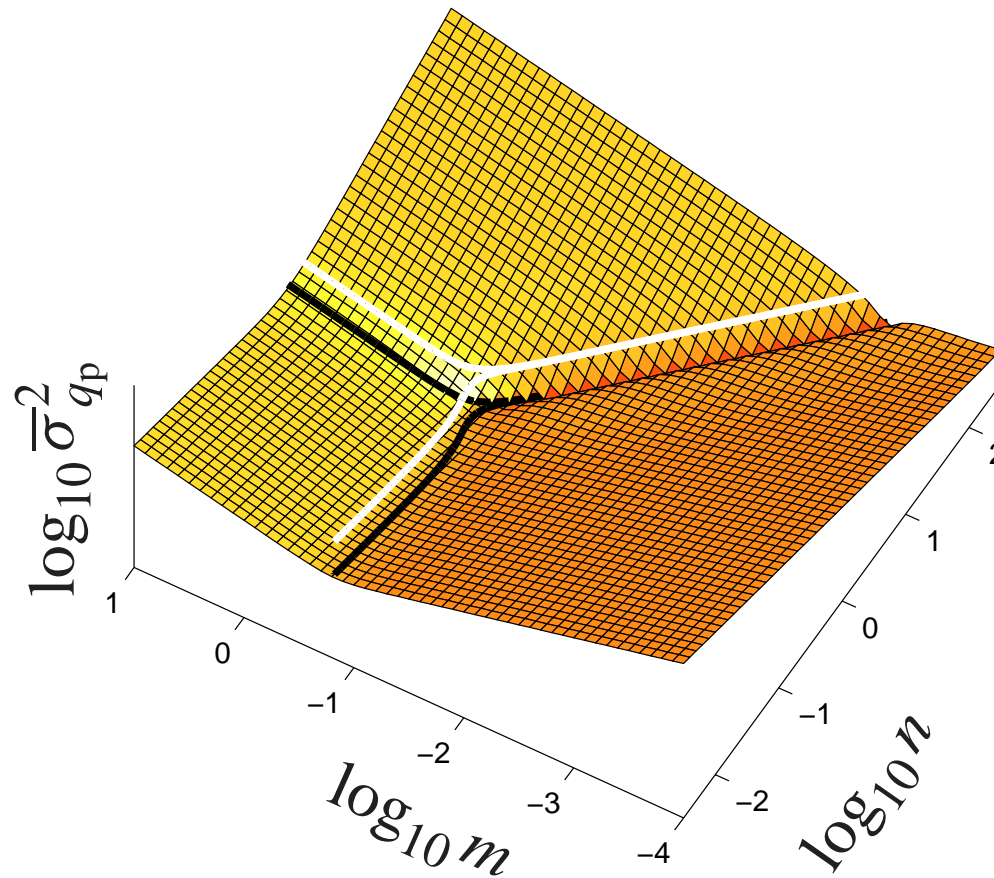
Sensitivity theory: Schöffler criterion

Relative Variances: $\bar{\sigma}_{R_1}^2 = \sigma_{R_1}^2 / R_1^2$

Schöffler Criterion: $\bar{\sigma}_{q_p}^2 \approx \sum_{x \in X} \left(S_x^{q_p} \right)^2 \bar{\sigma}_x^2, \quad X = \{R_i, C_j, \alpha_v\}$



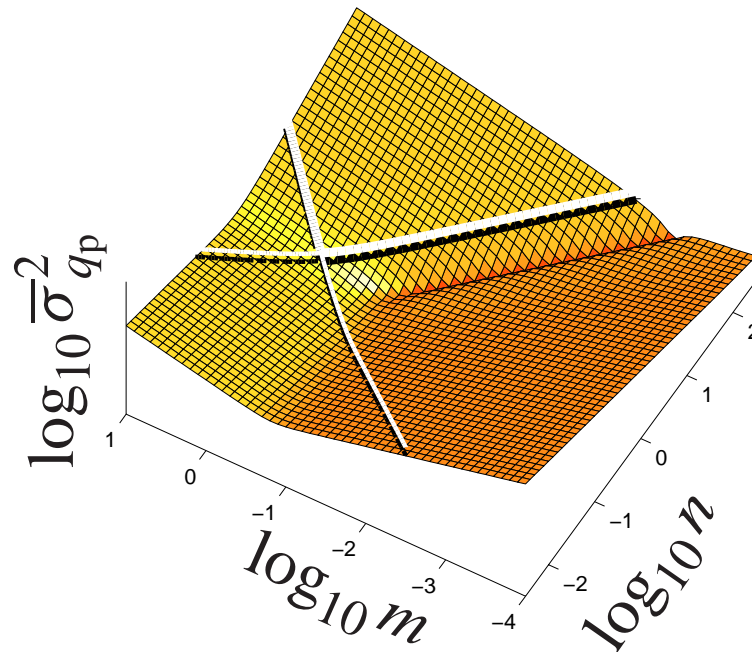
Gradients of the variance surface



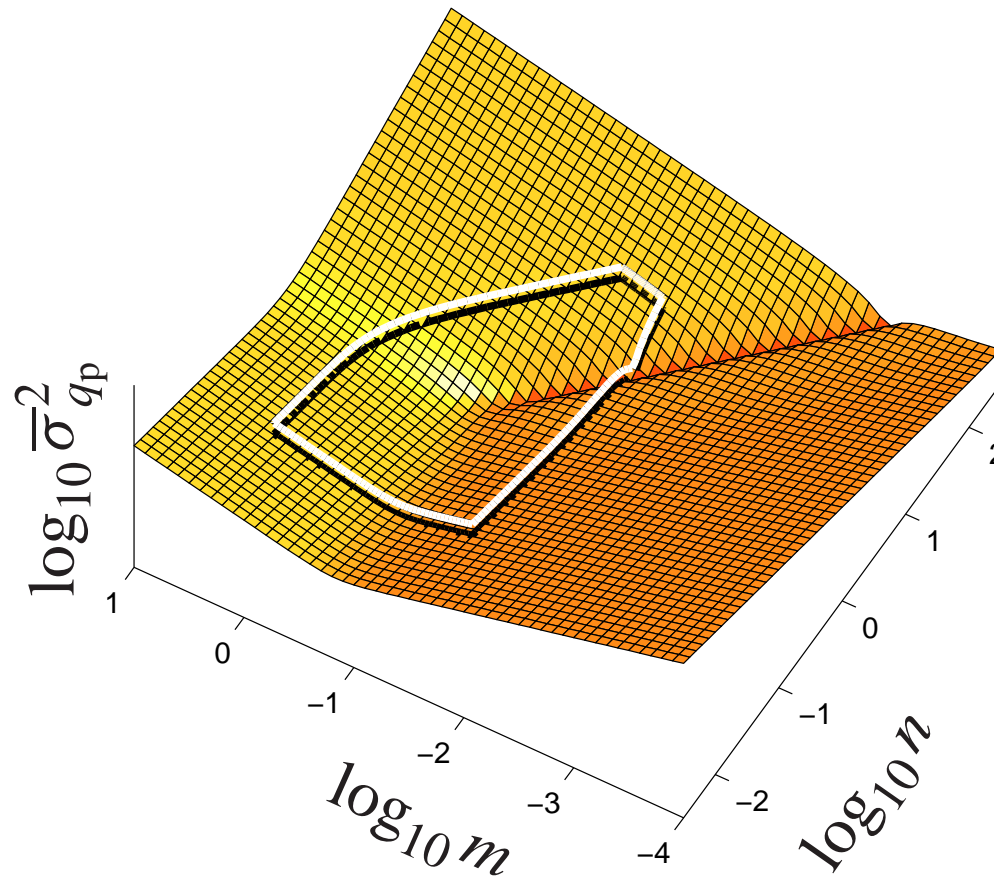
Coordinate transformation

$$\log_{10} x = \log_{10} m + \log_{10} n, \quad \log_{10} y = \log_{10} n - \log_{10} m$$

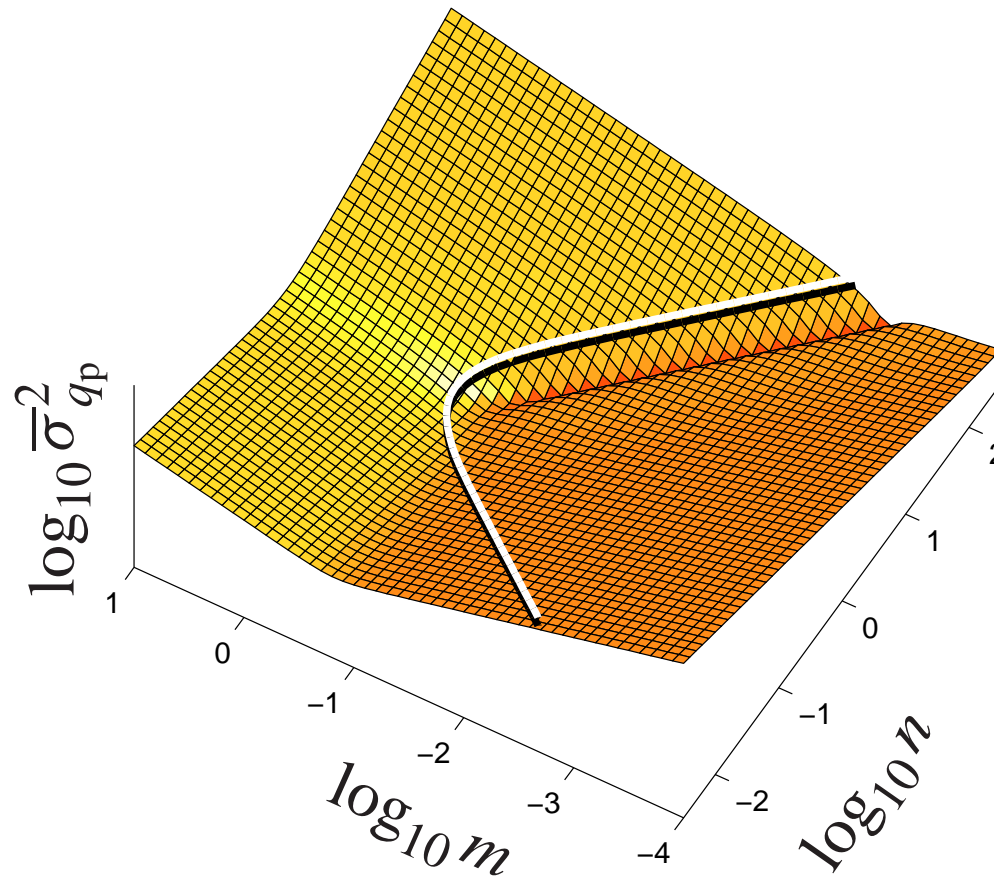
$$x = mn, \quad y = \frac{n}{m} \quad \text{with } m, n, x, y > 0$$



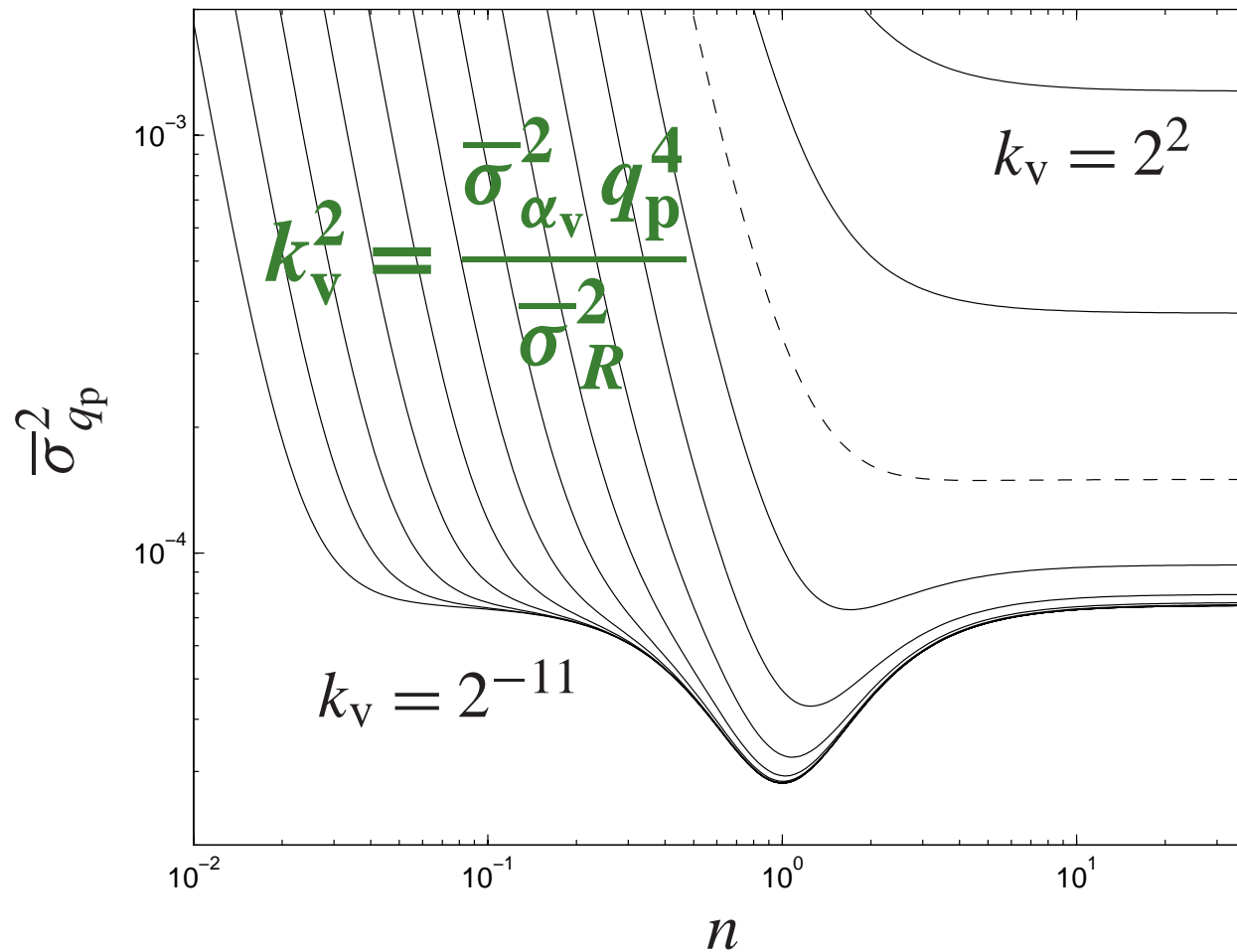
Boundary conditions



Unity-gain



Optimum resistor spread



Conclusion

Results: Limit on the ideal gain in the general case;
possible existence of a low-component-spread optimum
in the unity-gain case.

This allows us to build less expensive filters.

Paper: Design equations to find optimum m and n ;
mathematical proofs using root locus theory.

Alterations for Analogue IC Design:

$$\overline{\sigma}_{q_p}^2 \approx \sum_{x \in X} \left(S_x^{q_p} \right)^2 \overline{\sigma}_x^2, \quad X = \{R, C, m, n, \alpha_v\}$$